



Department of Chemical and Environmental Process Engineering

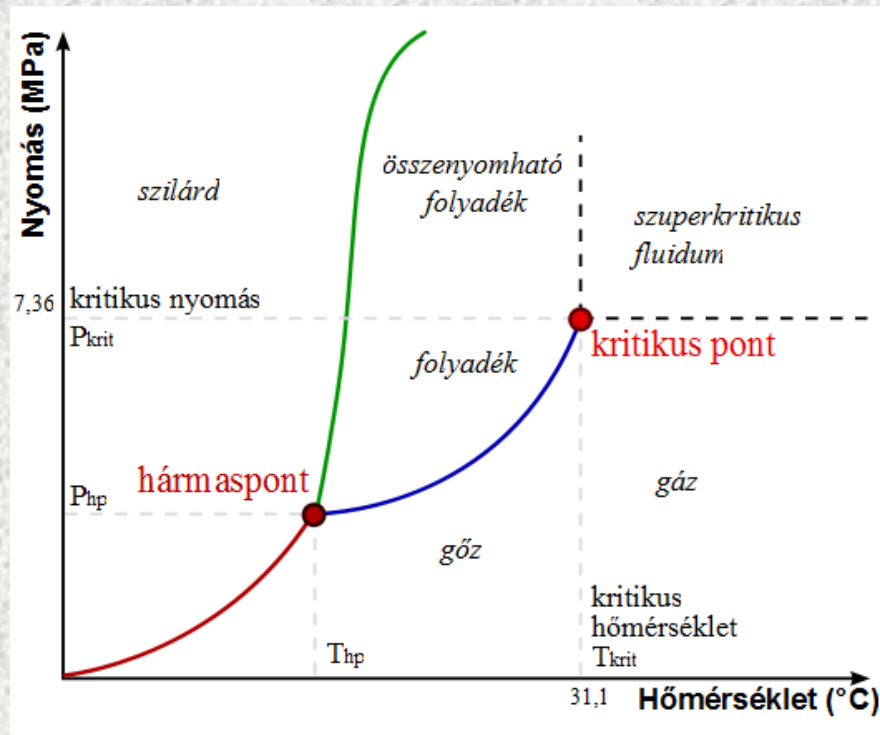
# Extraction

Chemical Unit Operations II.

Béla Simándi, Edit Székely

# Extraction

- I. Liquid-liquid extraction (Solvent extraction)
- II. Solid-liquid extraction (Leaching)
- III. Supercritical fluid extraction



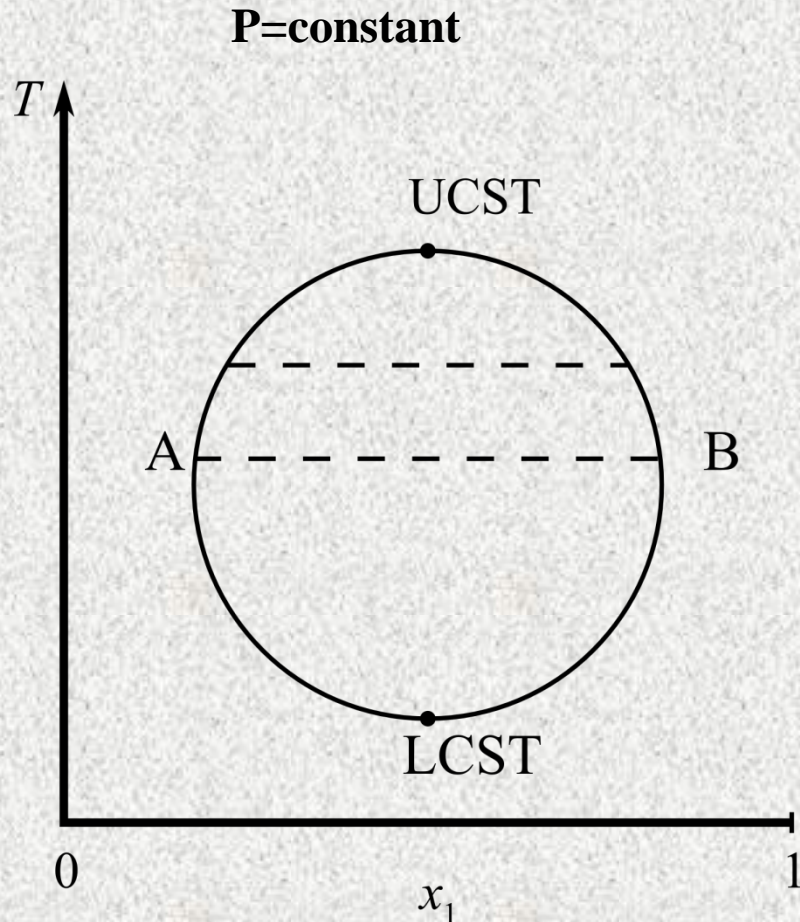
# Liquid-liquid extraction

## I. Applications

1. Hydrometallurgy
2. Inorganic processes
3. Petroleum industry
4. Pharmaceuticals
5. Waste waters

# II. Liquid-liquid equilibrium

## Binary systems



**Curve:** composition of saturated solutions of the two components.

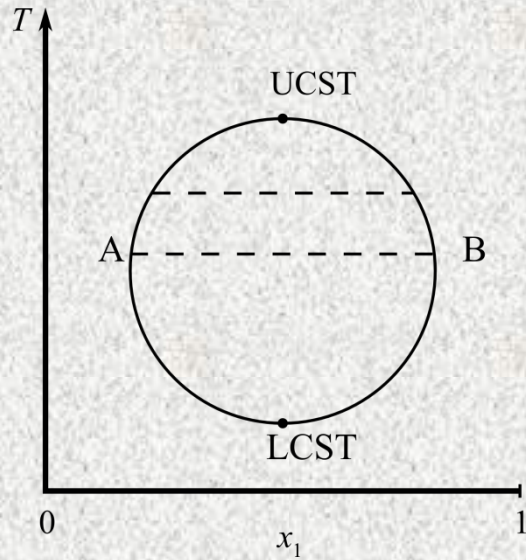
Area **enclosed** by the curve: two phase region;  
Area **outside** the curve: mixtures that are completely miscible.

**A, B:** composition of the phases in equilibrium.

Dashed line: **tie line**.

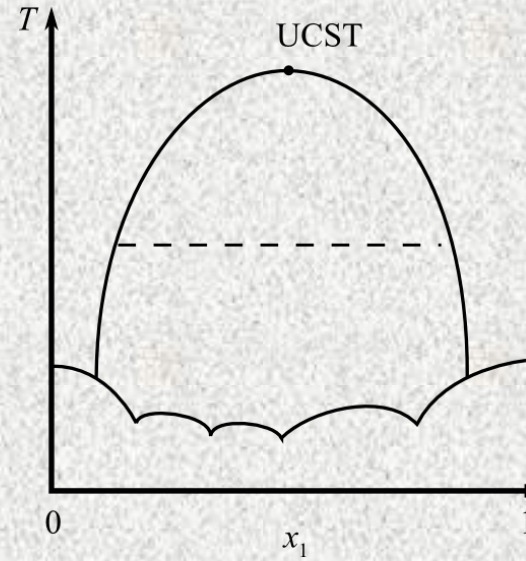
**UCST:** Upper Critical Solution Temperature.  
**LCST:** Lower Critical Solution Temperature.

# Binary systems

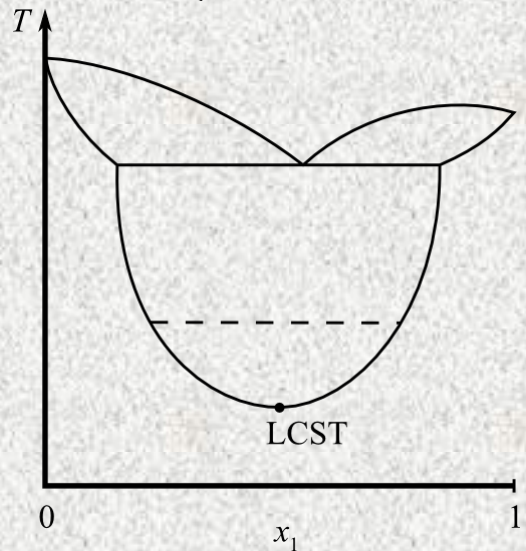


Type I.

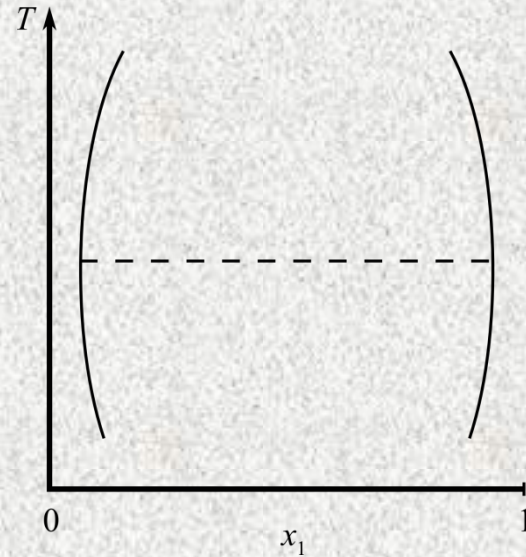
**P=constant**



Type II.



Type III.



Type IV.

# Ternary systems

**T=constant**

**P=constant**

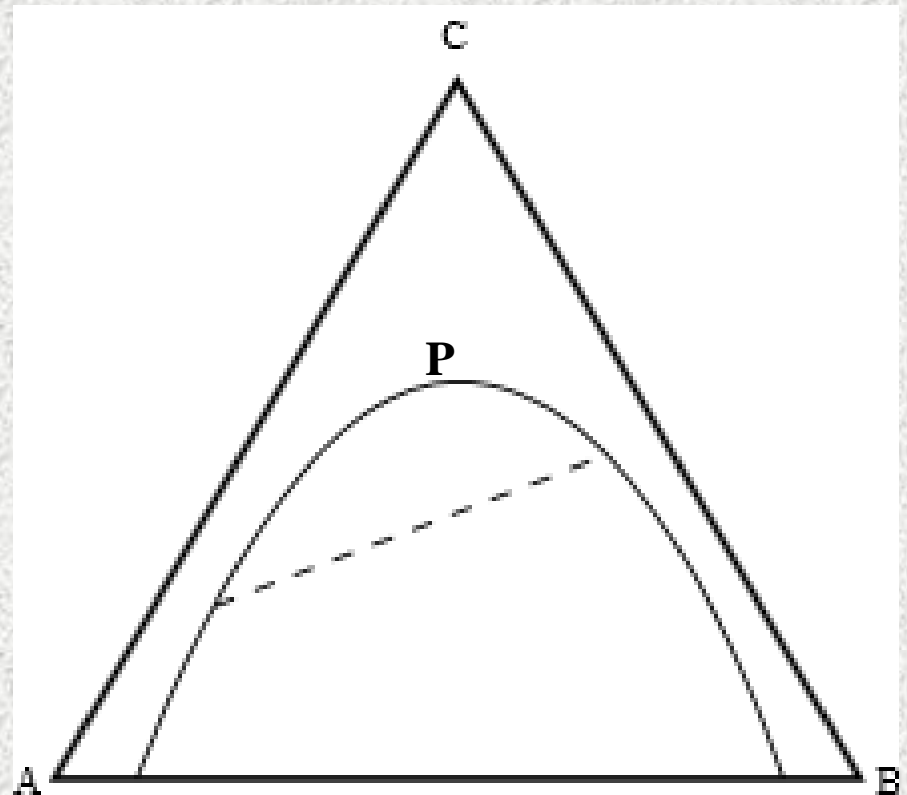
**A, B, C:** pure components.

Curve shown within the triangle: the boundary of the two phase region.

Ternary solubility curve=**binodal curve**.

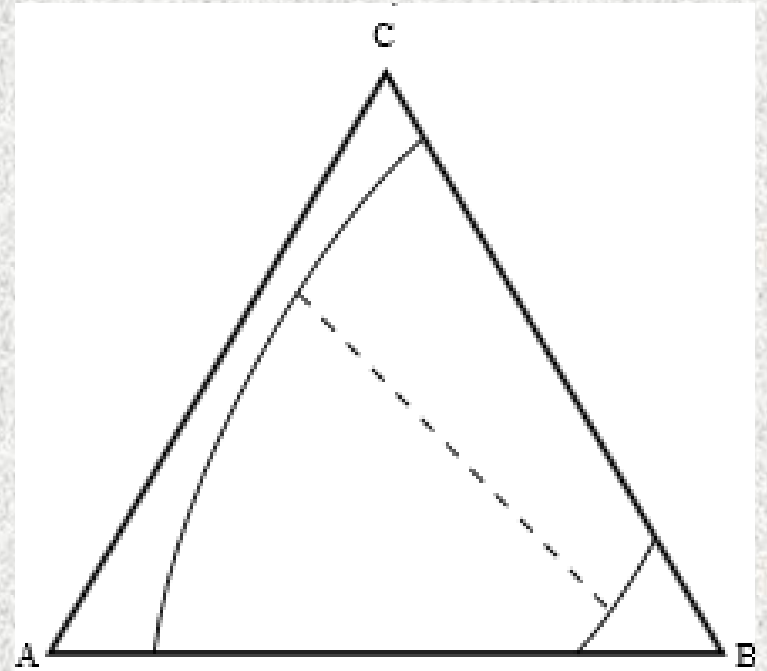
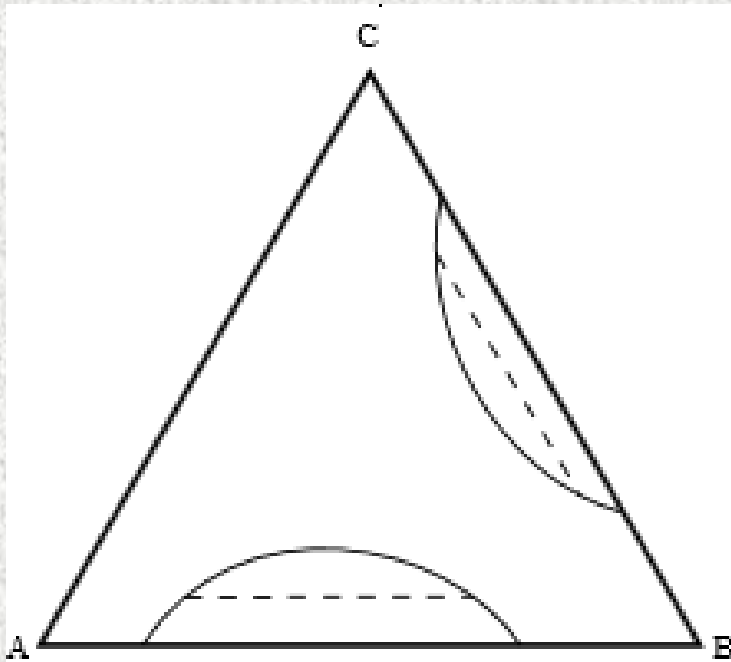
Dashed line = **tie line**.

**P:** plait point (limit of immiscibility).



**Type I.:** one partially miscible binary pair.

# Ternary systems



**Type II.:** two partially miscible binary pairs.

# III. Single stage extraction (batch extraction)

Theoretically ideal stage: where contact between phases is sufficiently intimate and maintained for a sufficient period of time that equilibrium is established.

Extract phase (E): solvent- rich phase

Raffinate phase (R): solvent-lean phase

## III/1. Simple stirred tank

*Equilibrium ratio for a simple ternary system:*

$$m = \frac{y}{x}$$

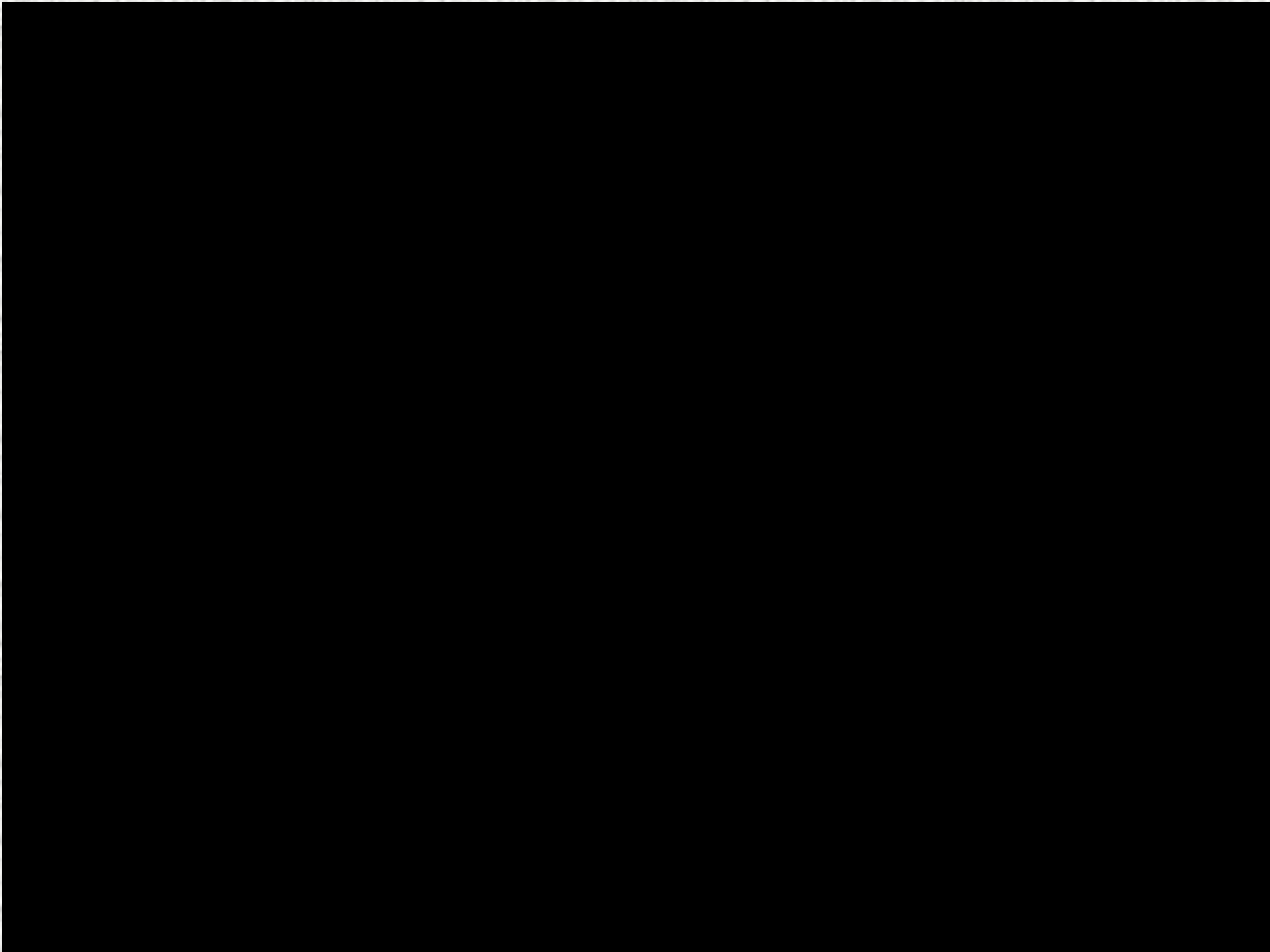
y: solute concentration in extract phase (wt%)

x: solute concentration in raffinate phase (wt%)

m: equilibrium ratio (distribution coefficient)







# III/1. Simple stirred tank



Total material balance:

$$m_{R_0} + m_{E_0} = m_{R_1} + m_{E_1}$$

Component balance for solute:

$$m_{R_0} * x_0 + m_{E_0} * y_0 = m_{R_1} * x_1 + m_{E_1} * y_1$$

$m_{R_0}$ : mass of the initial solution (kg)

$m_{E_0}$ : mass of the solvent (kg)

$m_{R_1}$ : mass of the raffinate (kg)

$m_{E_1}$ : mass of the extract (kg)

x, y: concentrations (wt%)

# III/1. Simple stirred tank

If the solvent and diluent are immiscible and the concentration of solute is low:

$$f = \frac{m_{E0}}{m_{R0}} = \frac{m_{E1}}{m_{R1}} = \text{constant}$$

$$y_1 = m * x_1 \quad \longrightarrow \quad x_0 + f * y_0 = x_1 + f * y_1 = x_1 + f * m * x_1$$

$$E = \frac{m_{E1} * y_1}{m_{R1} * x_1} = f * m$$

Extraction factor

$$x_0 + f * y_0 = x_1 * (1 + E)$$

$$x_1 = \frac{x_0}{1 + E} + \frac{E * \left(\frac{y_0}{m}\right)}{1 + E}$$

If  $y_0=0$  (neat solvent)

$$\left\{ \begin{array}{l} x_1 = \frac{x_0}{1 + E} \end{array} \right.$$

## III/2. Multiple-extraction

The raffinate from the first stage is extracted with fresh solvent of the same composition in successive stages.

General solution (if neat solvent is used):

First stage  $x_1 = x_0 * \frac{1}{1 + E}$

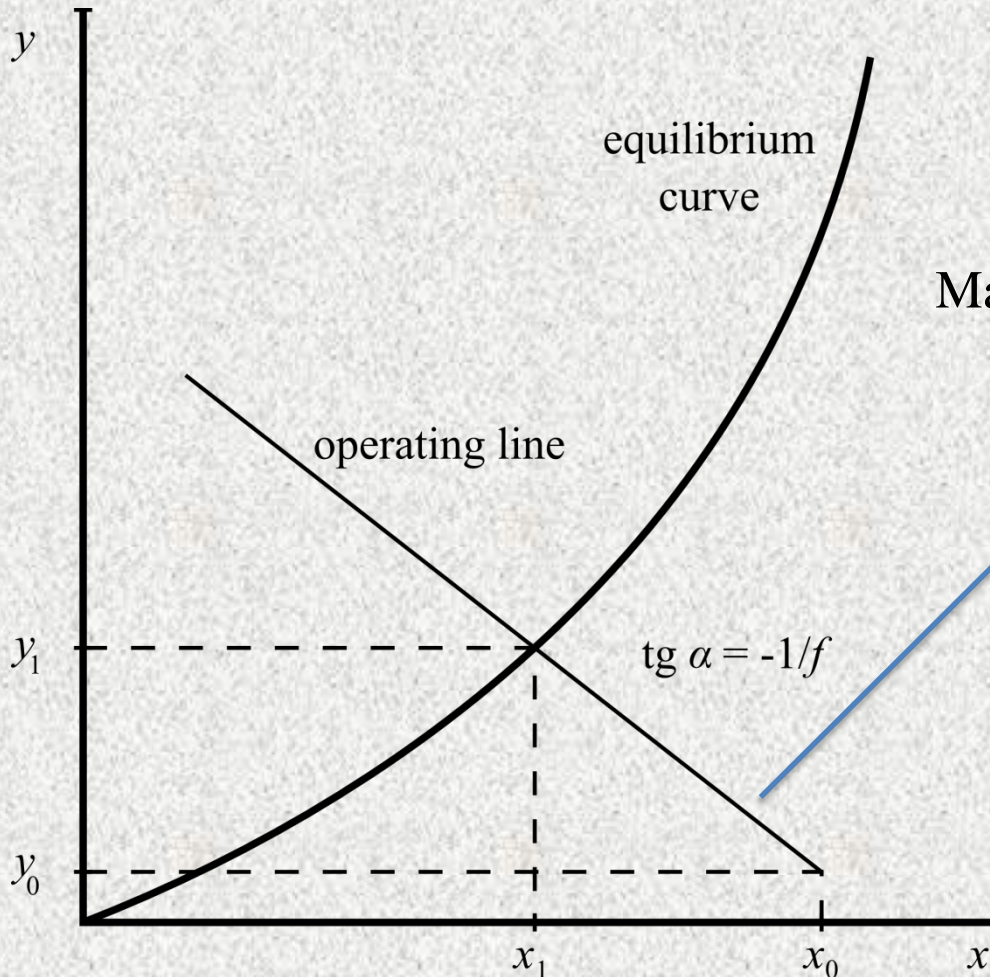
Second stage  $x_2 = x_1 * \frac{1}{1 + E} = x_0 * \frac{1}{(1 + E)^2}$

Third stage  $x_3 = x_2 * \frac{1}{1 + E} = x_0 * \frac{1}{(1 + E)^3}$

$n^{\text{th}}$  stage  $x_n = x_0 * \frac{1}{(1 + E)^n}$

## III/2. Multiple-extraction

If liquids are completely immisible or at least their solubility does not change over the range of concentration of distributed substance:

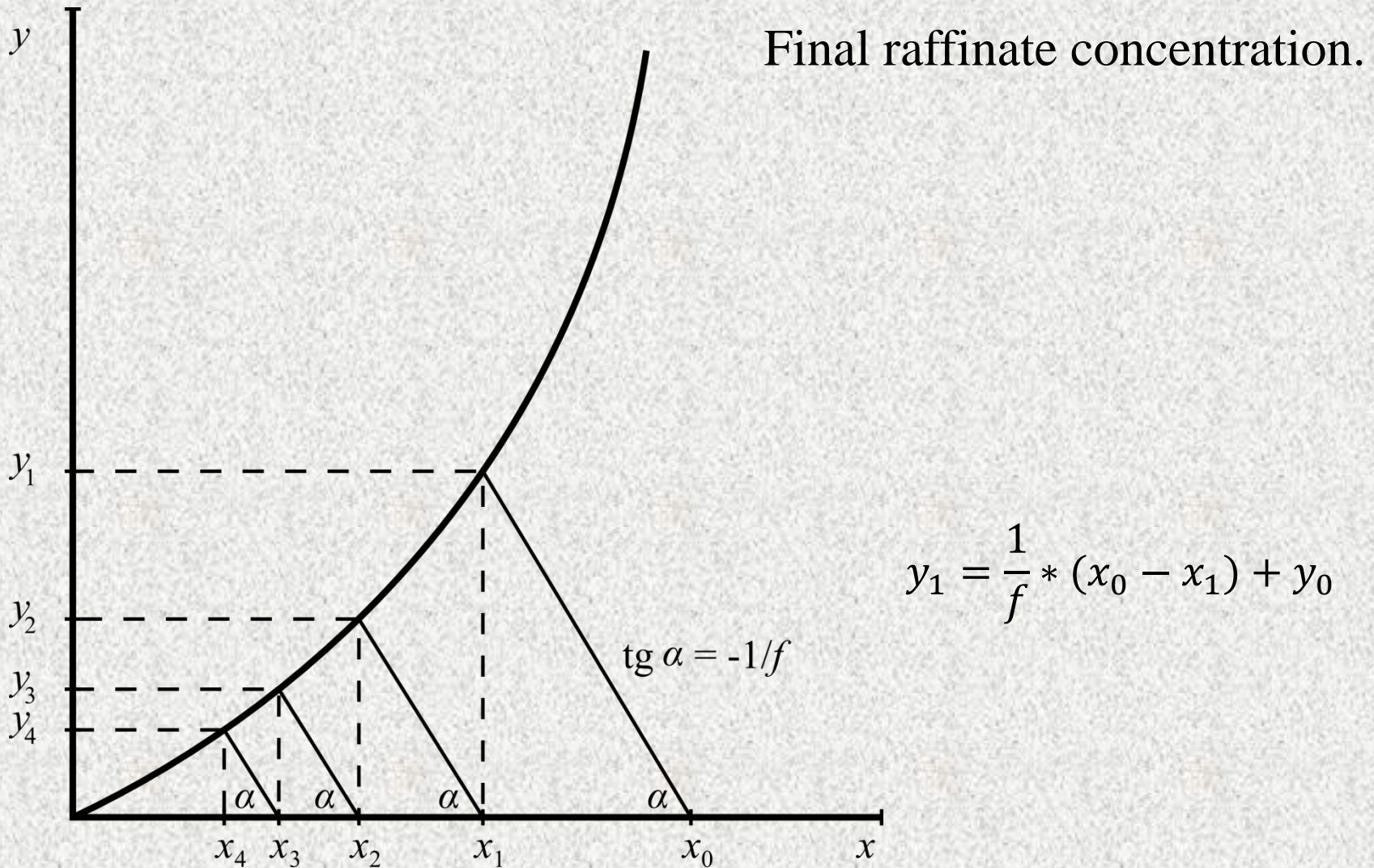


Material balance equation gives:

$$y_1 = \frac{1}{f} * (x_0 - x_1) + y_0$$

$$tga = -\frac{1}{f}; \text{ through } (x_0, y_0)$$

## III/2. Multiple-extraction



# III/2. Multiple-extraction

## Triangular diagram

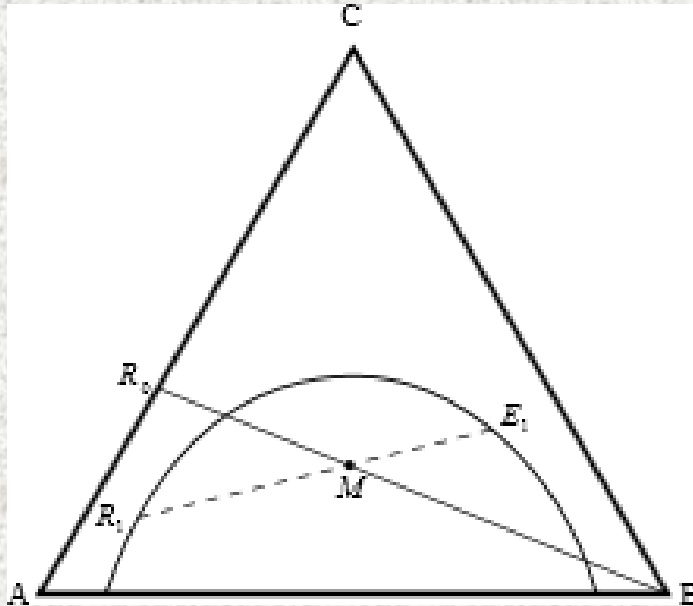
- If 'f' and 'm' depend on the composition.

Material balance:

$$m_{R_0} + m_{E_0} = m_{R_1} + m_{E_1}$$

$$m_{R_0} * x_0 + m_{E_0} * y_0 = m_{R_1} * x_1 + m_{E_1} * y_1$$

$x_{M_1}$ : overall composition of the ternary mixture, **M1** point can be located by the lever-arm rule.



Calculation:

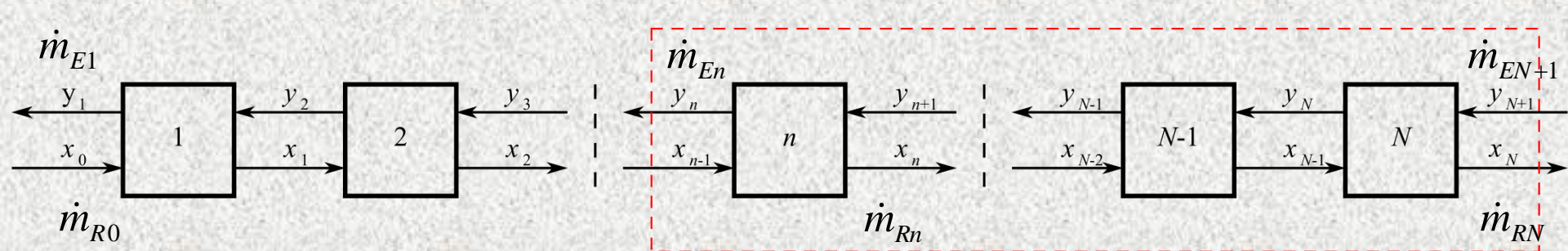
$$x_{M_1} = \frac{m_{R_0} * x_0 + m_{E_0} * y_0}{m_{R_0} + m_{E_0}}$$

$$x_{M_1} = \frac{m_{R_1} * x_1 + m_{E_1} * y_1}{m_{R_1} + m_{E_1}}$$





# III/3. Continuous extraction



$\dot{m}_{En}$  : extract mass flowrate leaving stage  $n$  (kg/s)

$y_n$  : solute concentration in  $\dot{m}_{En}$  (mass fraction)

$\dot{m}_{Rn}$  : raffinate flowrate leaving stage  $n$  (kg/s)

$x_n$  : solute concentration in  $\dot{m}_{Rn}$  (mass fraction)

$N$  : number of equilibrium stages (-)

# III/3. Continuous extraction

- If the solvent and diluent are completely immiscible and  $m$  is constant:

$$\frac{x_N - \frac{y_{N+1}}{m}}{x_0 - \frac{y_{N+1}}{m}} = \frac{E - 1}{E^{N+1} - 1}$$

$$E = f * m \quad \text{extraction fraction}$$

$$f = \frac{\dot{m}_E}{\dot{m}_R} \quad \text{flowrate ratio}$$

If  $E=1 \longrightarrow \frac{x_N - \frac{y_{N+1}}{m}}{x_0 - \frac{y_{N+1}}{m}} = \frac{1}{N + 1}$  Kremser (1930)

- If the solvent and diluent are completely immiscible or at least their solubility does not change over the range of concentration of distributed substance: **McCabe-Thiele analysis**.

$$\dot{m}_R * x_{n-1} + \dot{m}_E * y_{N+1} = \dot{m}_R * x_N + \dot{m}_E * y_n \longrightarrow y_n = \frac{1}{f} * (x_{n-1} - x_N) + y_{N+1}$$

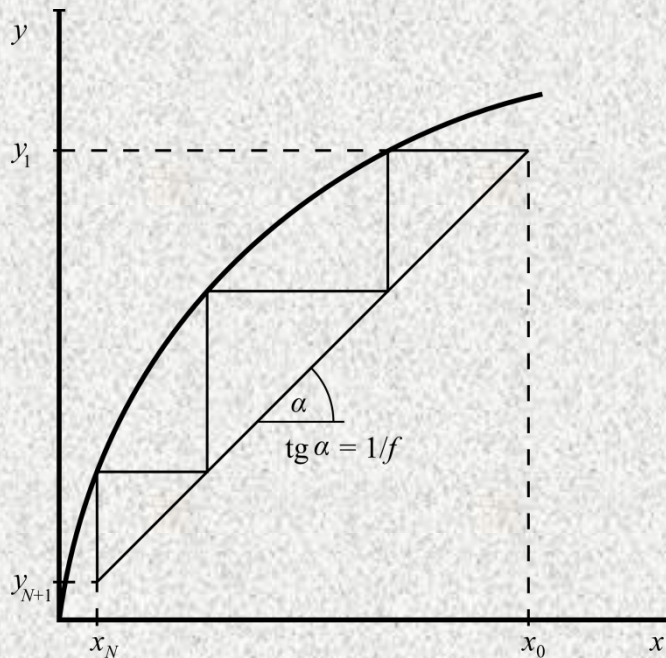
Operating line

Raffinate and extraction rates are constant.



# III/3. Continuous extraction

- If 'f' changes only because of transfer of solute from raffinate phase to the extract phase the same diagram and method can be used.



$$y = \frac{\textit{solute}}{\textit{solute} - \textit{free solvent}}$$

$$x = \frac{\textit{solute}}{\textit{solute} - \textit{free diluent}}$$

} New coordinate system.

Total flow rates:

$\dot{m}_E$ : solute-free extract (usually neat solvent)

$\dot{m}_R$ : solute-free raffinate (usually neat diluent)

- Triangular diagrams can be used for partially miscible systems!
- System of more than three components require computers for solution of their model equations.

# IV. Selection of solvent in extraction

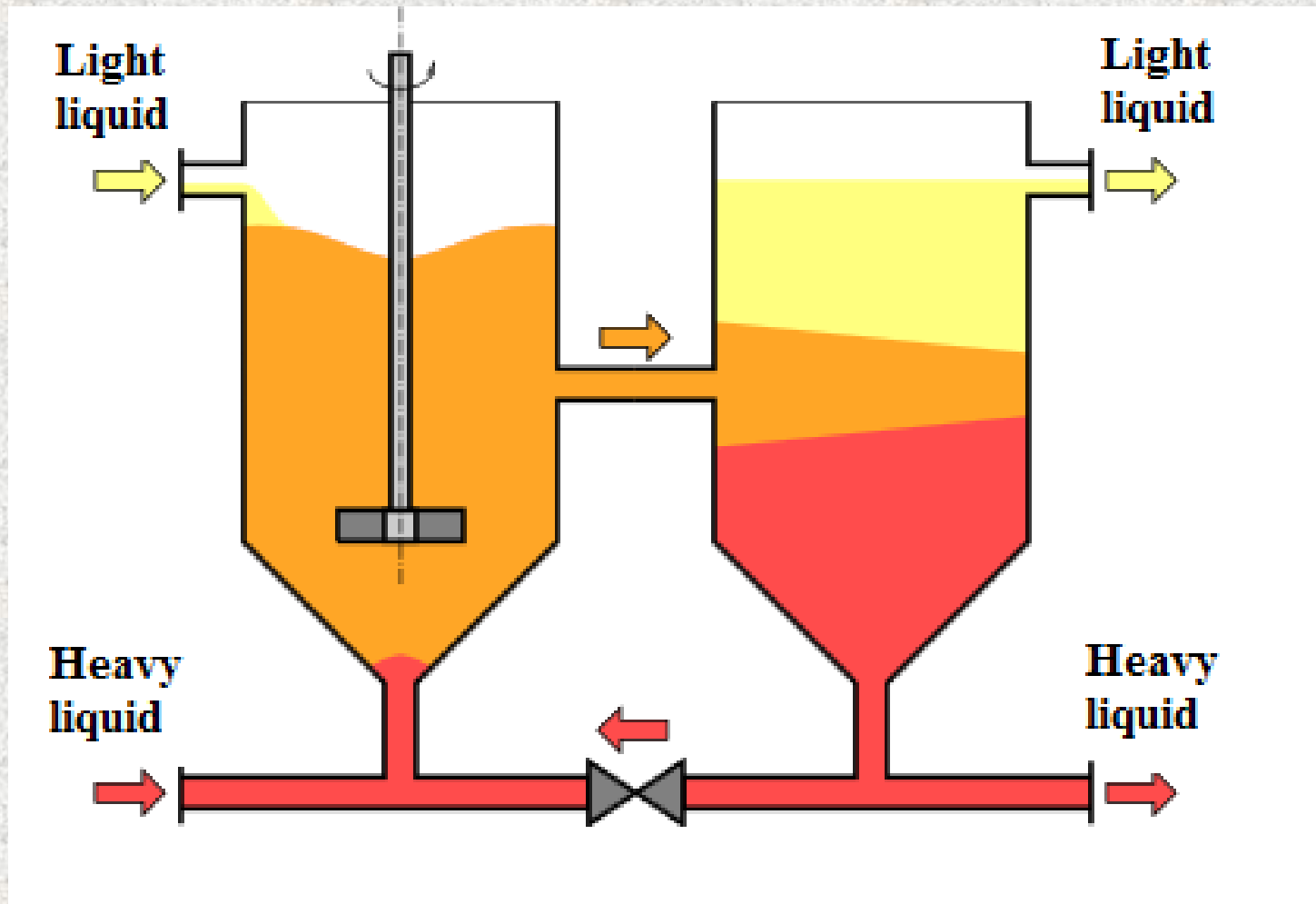
The proposed solvent must form a separate phase from the feed solution and should be able to extract the solute from the feed solution.

1. Distribution coefficient ( $m$ )
2. Solubility
3. Density ( $\Delta\rho > 150 \text{ kg/m}^3$ )
4. Interfacial tension
5. Viscosity
6. Chemical reactivity and stability
7. Vapour pressure
8. Flammability
9. Toxicity
10. Cost analysis

# V. Equipment

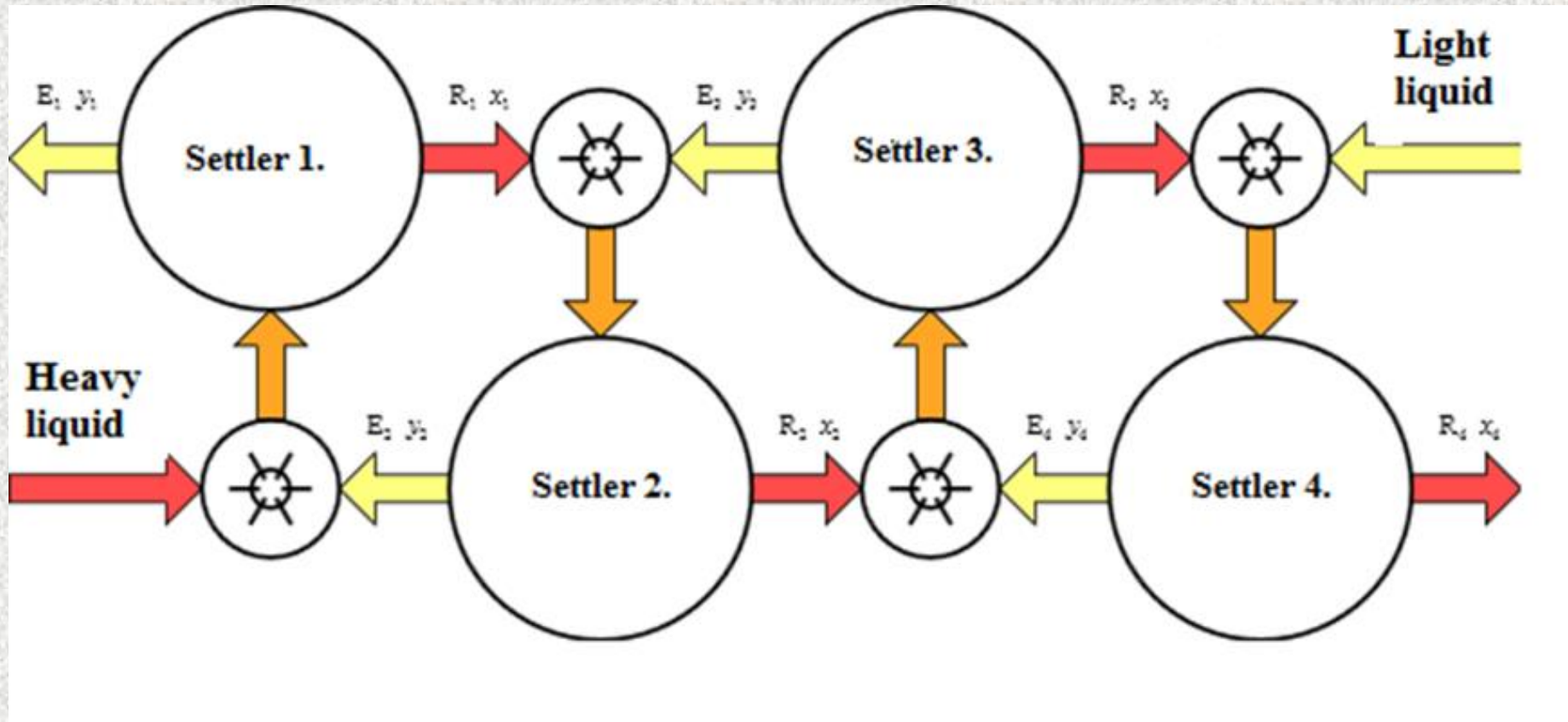
1. Mixer-settler or a series of mixer-settlers
2. A column, which may be agitated or pulsed
3. Some other contactor such as a centrifugal device

# V/1. Mixer-settler



The separating efficiency is proportional to the area of the phase interface. 23

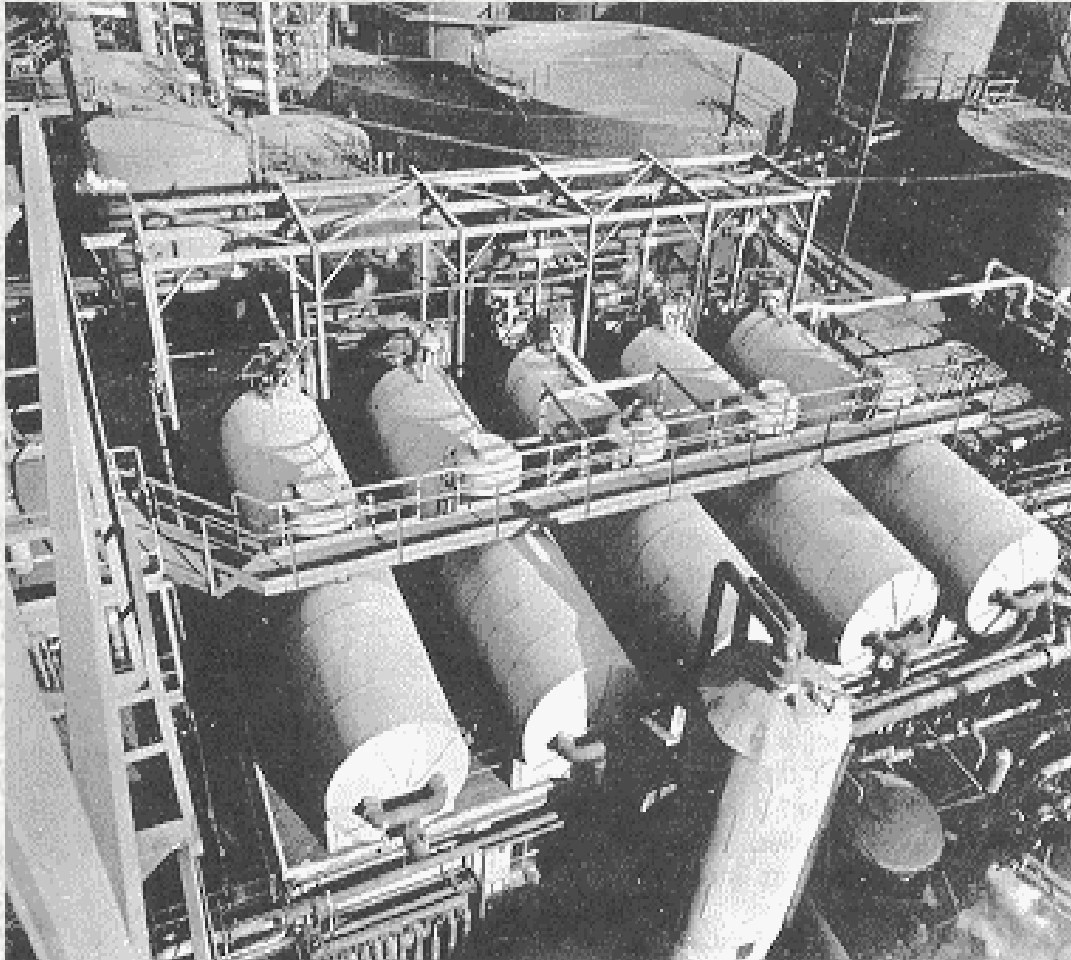
# V/1. Mixer-settler cascade



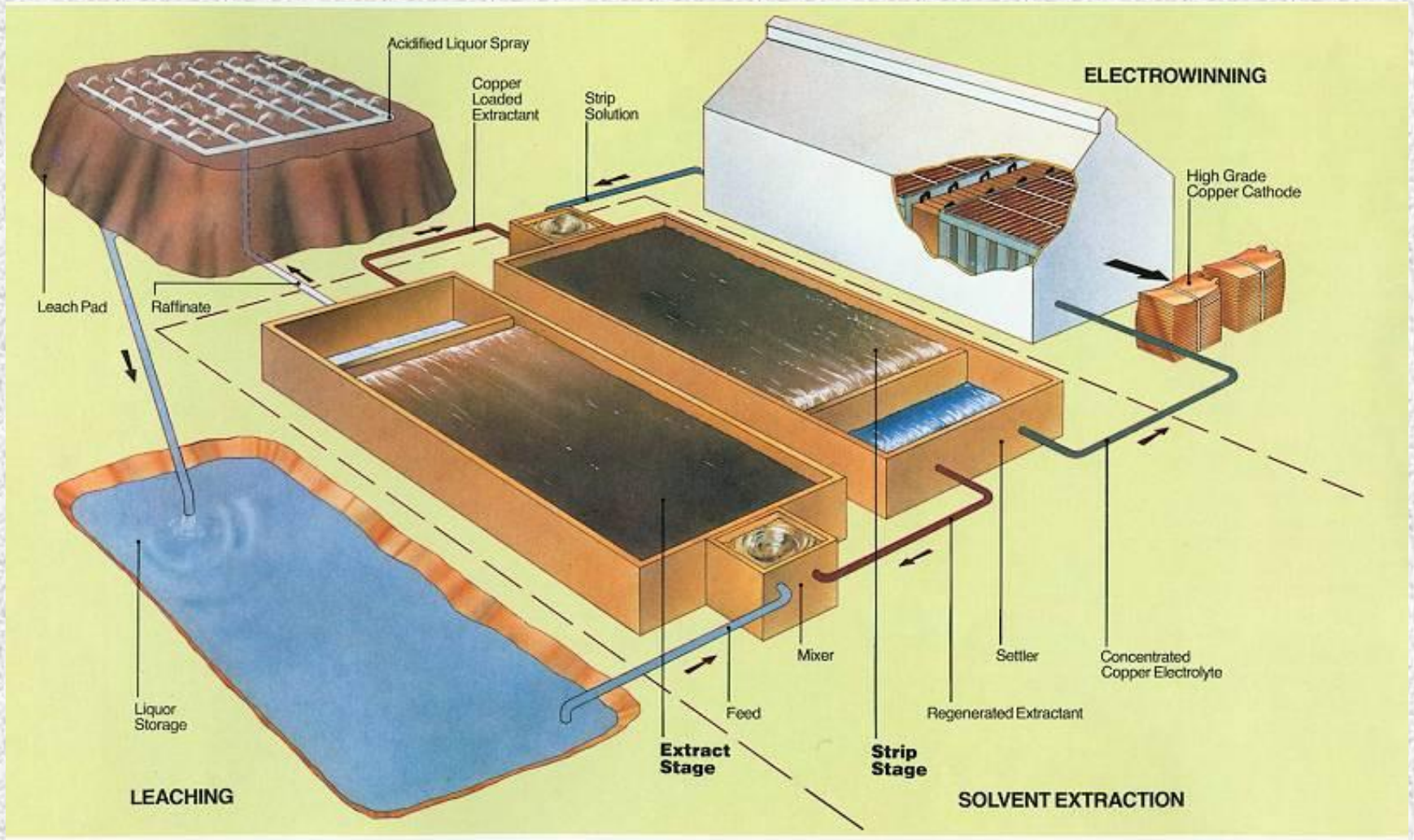
Large hold up volumes, long residence time, large physical size.



# V/1. Mixer-settler cluster



# V/1. Copper's extraction in Mixer-settler

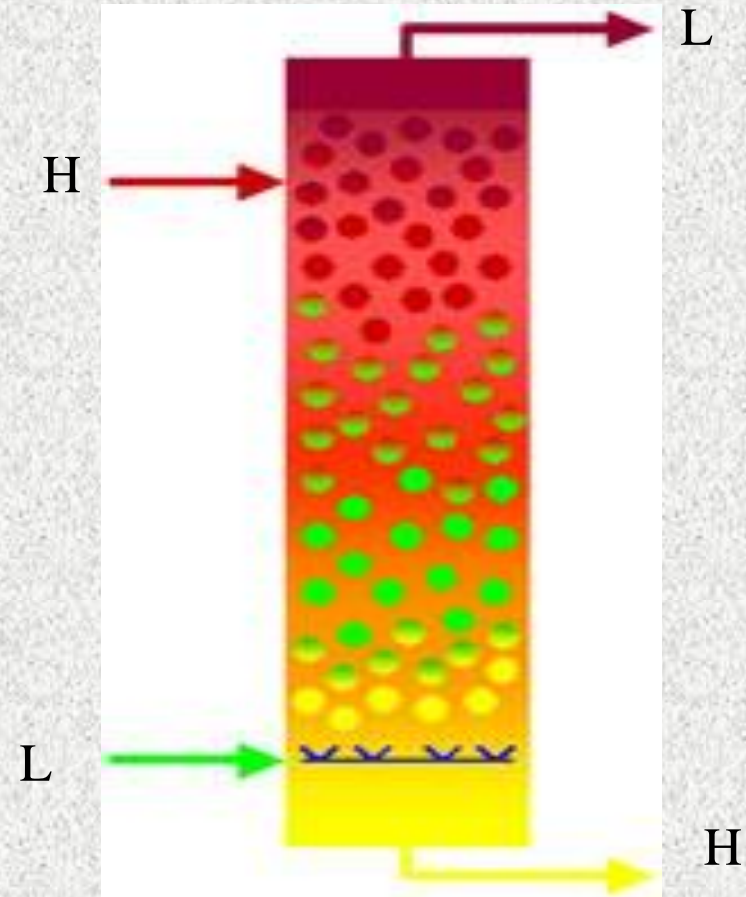


# V/2. Columns without energy input

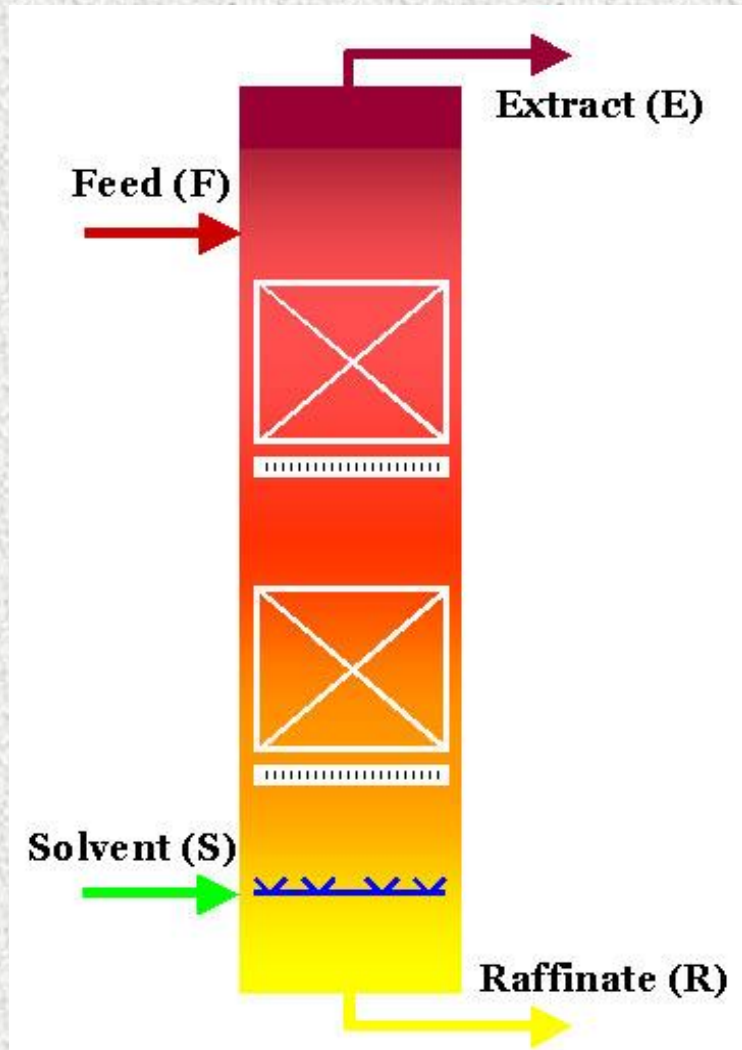
## a.) Spray column

Simplicity  
High throughput  
Low cost

Application: little in industry.

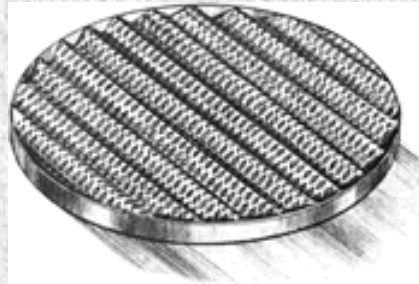
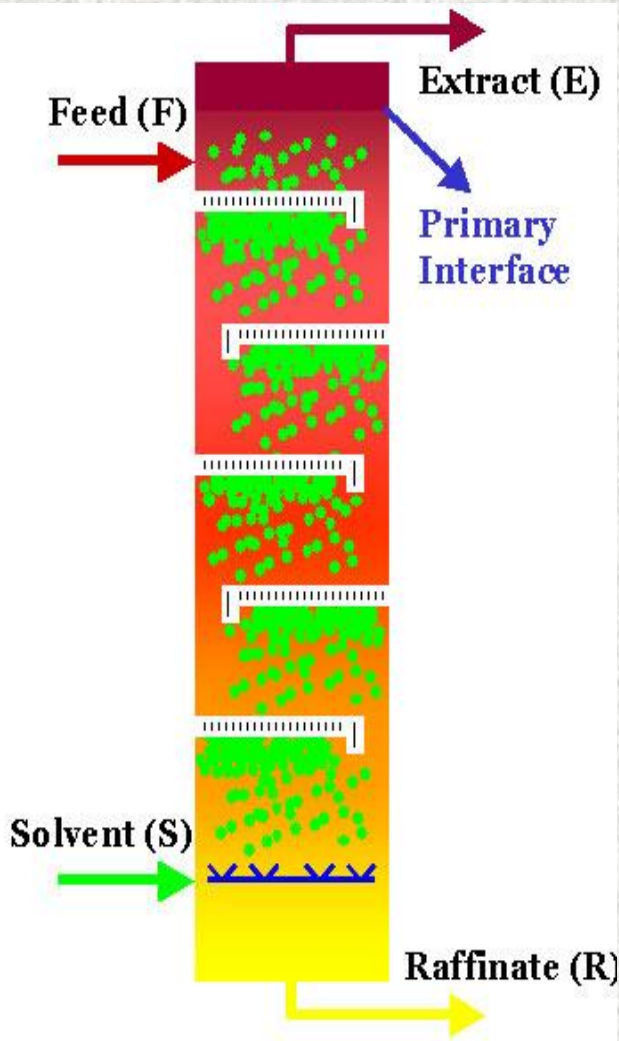


## b.) Packet columns



- The most purposes random packing;
- The packing should be wetted by the continuous phase.

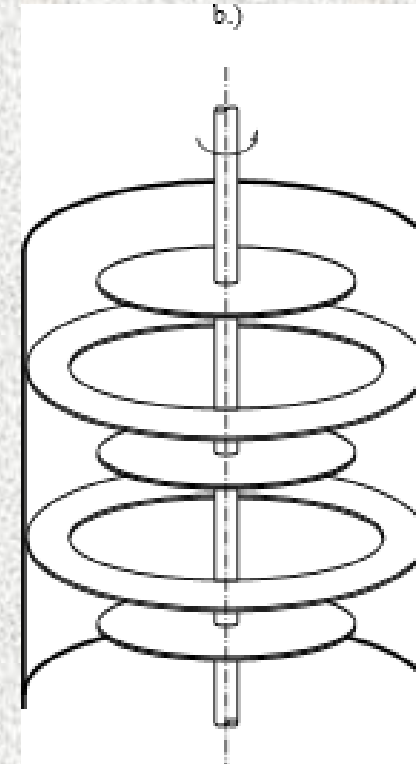
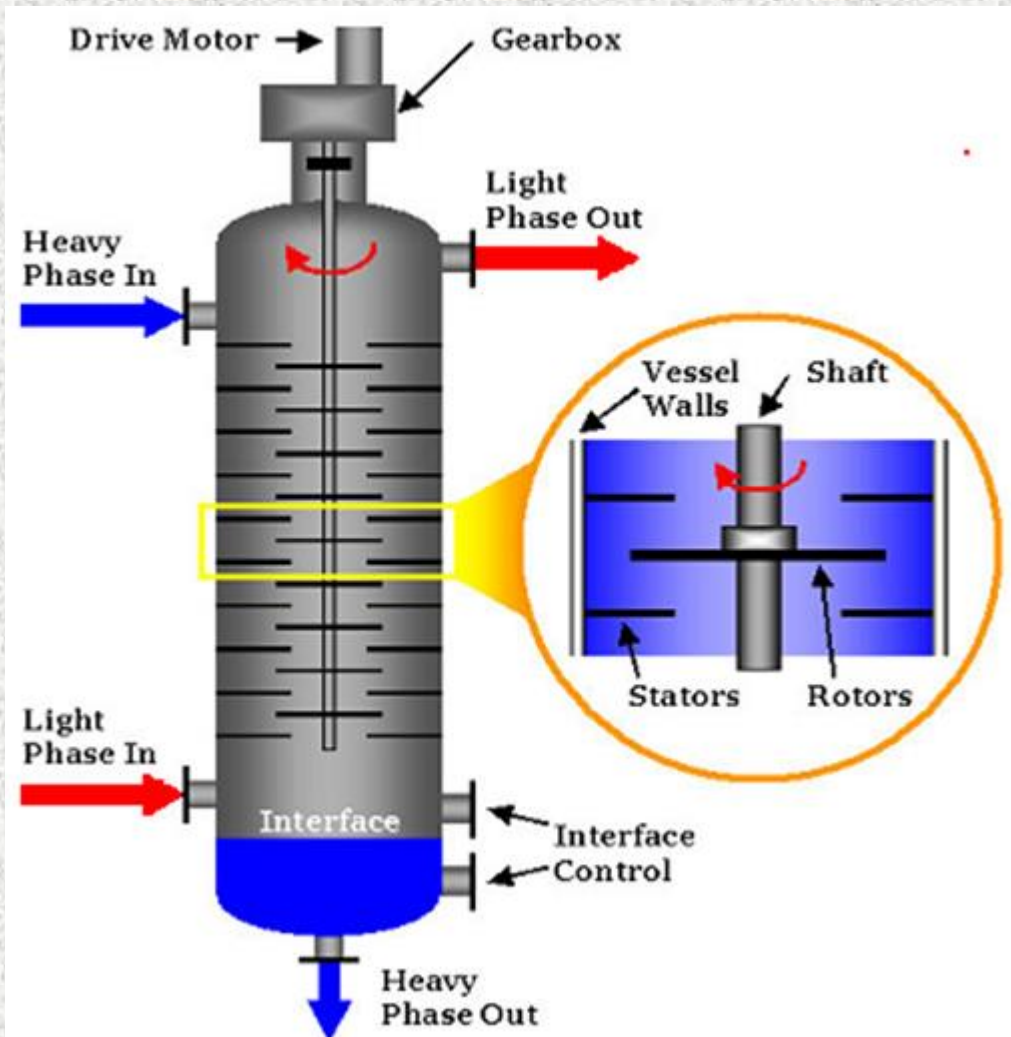
## c.) Sieve-Trey column



Application: in petroleum industry.

# V/3. Columns with energy input

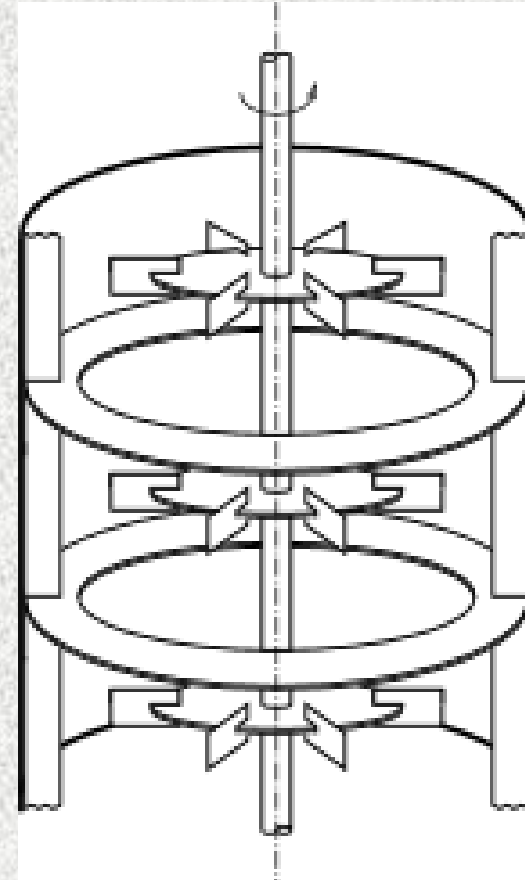
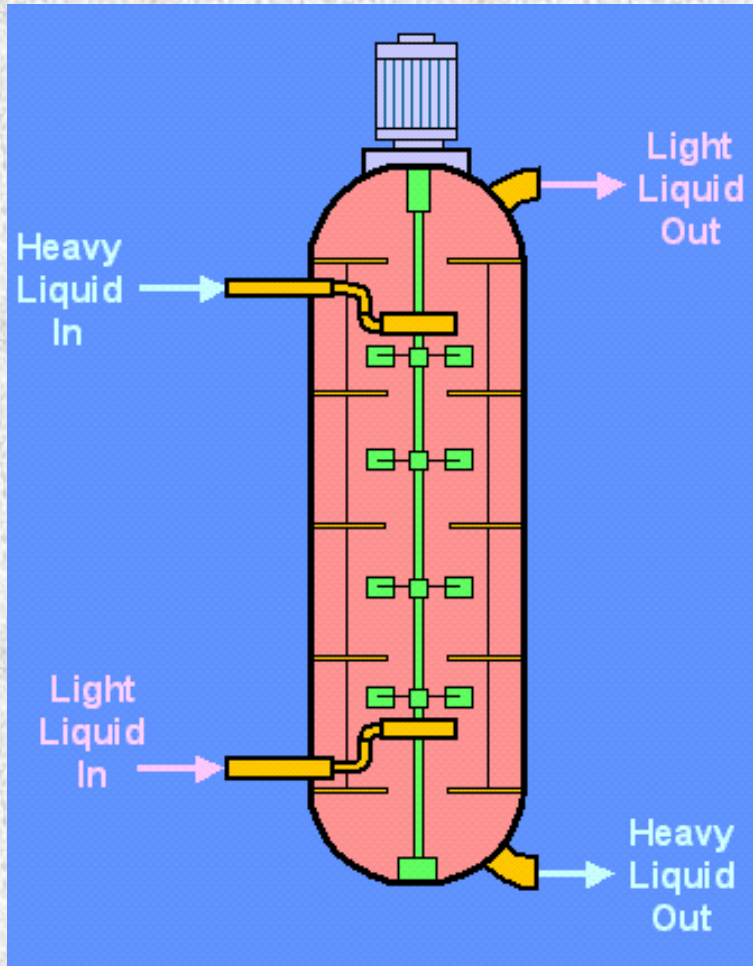
## a.) Rotating Disc Contactor (RDC)



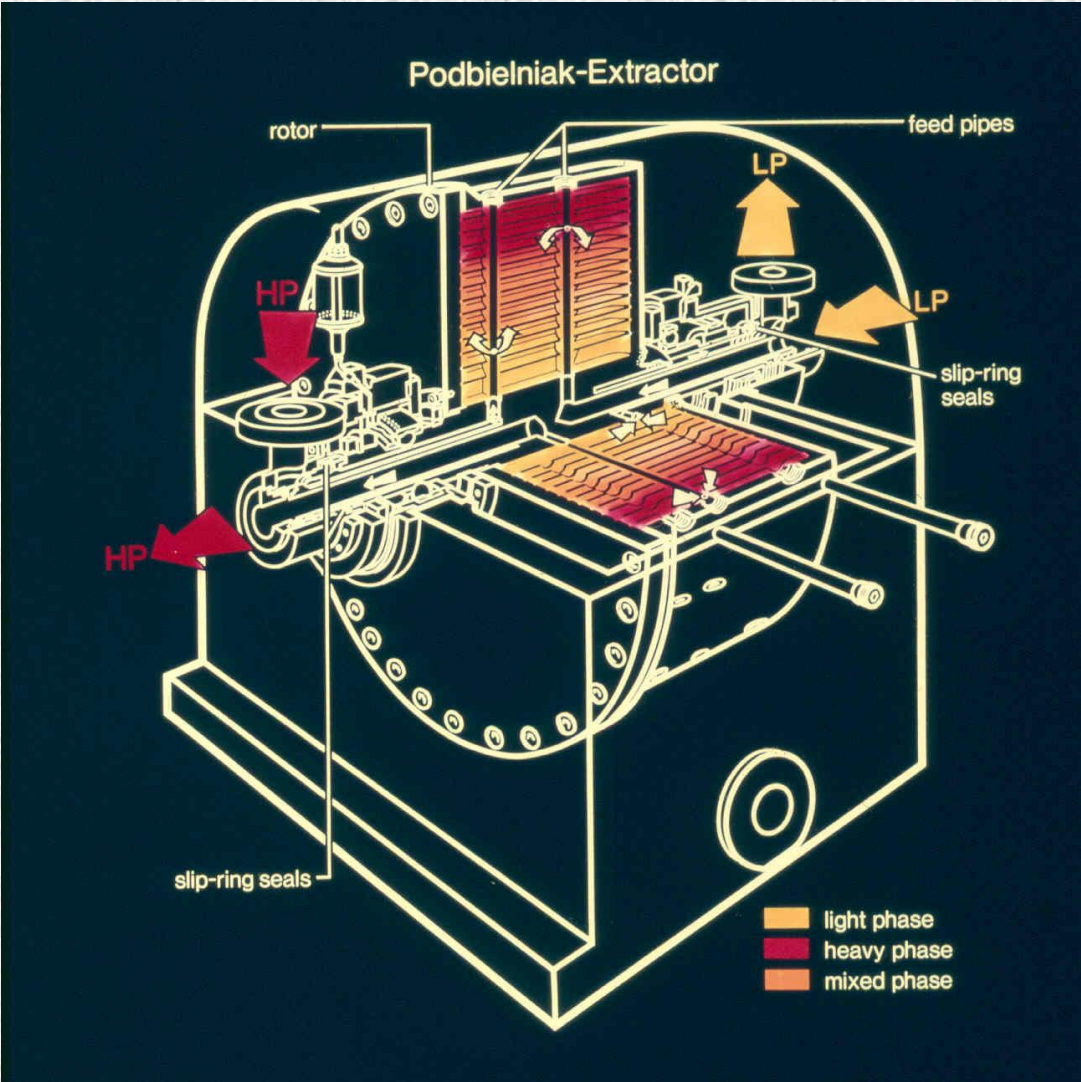
Shell  
1948

Application: in petroleum and chemical industries, waste water treatment.

## b.) Oldshue-Rushton column (1952, USA)



# Centrifugal Extractor (Podbielniak-Extractor)

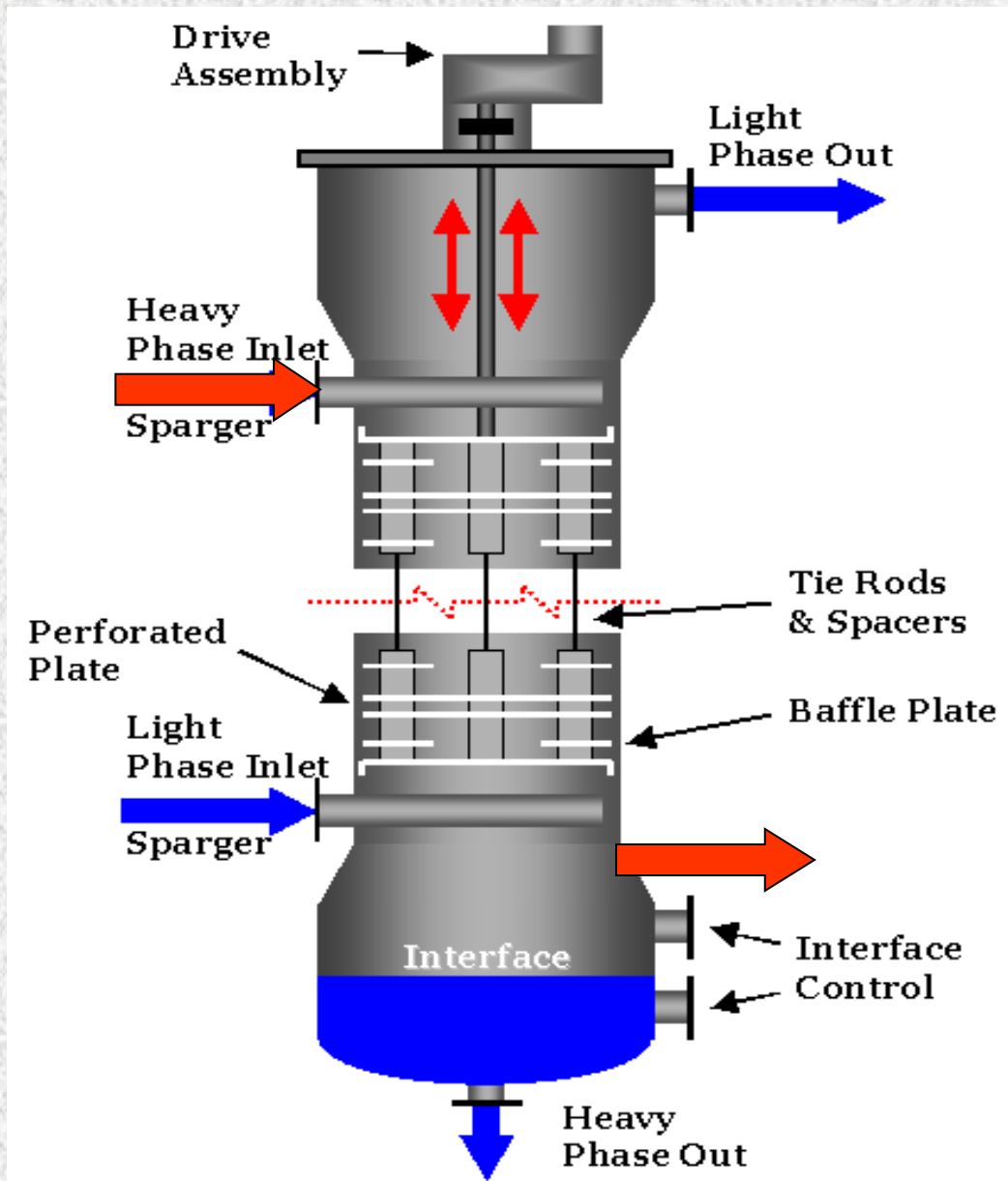




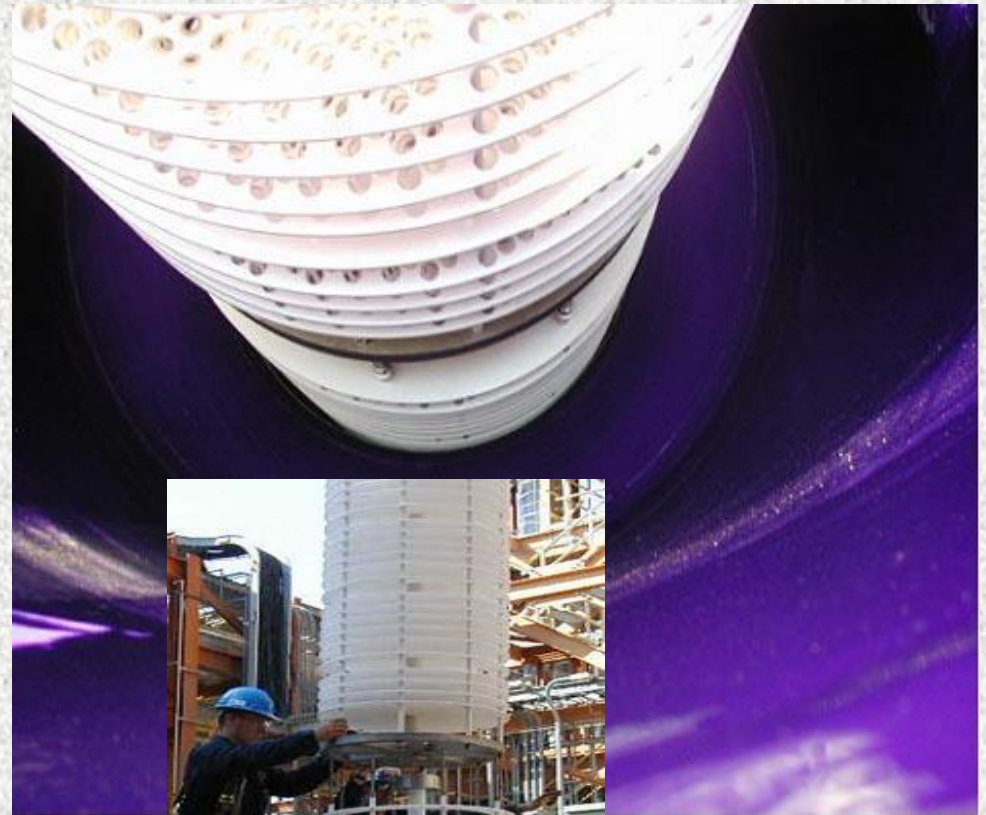
# Centrifugal extractor (Podbielniak-Extractor)



# Karr column



# Karr column



**Thank you for your attention!**